Review on Removal Techniques for Phenolic Compounds

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Abstract

Realising the growing demand of energy and resources conservation, it has become indispensable to devise a treatment technology which is both economical and environment friendly. The United States Environmental Protection Agency recommends level of Phenol in surface water limited to 0.5 mg/L. The permissible limit for discharge of Phenol in drinking water defined by US-EPA (Ohio EPA 2002), European Union (Busca et al., 2008) and MINAS of CPCB, India is 0.5 mg/L.

Conventionally, phenols are treated using chemical oxidation (C.O), bio-oxidation (B.O) or adsorption (Siemens Water Technologies Corp., 2009) where all the methods have their own advantages and disadvantages.

Introduction

The exposure to Phenol causes skin irritation and necrosis. It damages kidney, liver, muscles and eyes. The main reason behind the skin damage is the coagulation due to reaction of Phenol with amino acids present in the keratin of the epidermis and collagen in inner skin. Its harmful effects are characterised by dryness in throat and mouth, dark coloured urine and strong irritation in mucous membranes (Michalowicz and Duda, 2007). Their presence even in low concentration can cause hindrance in use and/or reuse of water. This results in unpleasant taste and odour of water and imparts negative effects on different biological processes (Dabrowski et al., 2005).

1. Phenol removal

2.1 **Techniques for phenol removal**

The removal techniques can be broadly classified into *Batch* and *Continuous* processes. The technologies used for its removal are adsorption on activated carbon (Ahmaruzzaman & Sharma., 2005), using a disinfectant like Chlorine Dioxide (ClO2) (Siemens Water Technologies Corp, 2009). Phenols may be treated by chemical oxidation or bio-oxidation.

Wastewater with Phenol concentration 500-2000 mg/l or higher is considered good for Phenol recovery in solvent extraction and adsorption on granular activated carbon (National Recommended Water Quality Criteria., 1999). Table 1 provides criteria for selecting removal technique based on phenol concentration in wastewater (National Recommended Water Quality Criteria., 1999).

Table 1 Criteria for selecting removal technique for phenol from wastewater

| Criteria | | | | Remarks | | | |
|---------------------------|---------|-----|--------|---|--|--|--|
| Intermediate | or | low | Phenol | Solvent extraction not good option | | | |
| concentration | | | | | | | |
| Economics not major issue | | | | Adsorption on activated carbon or biological removal better | | | |
| | | | | choice | | | |
| Phenol < 5 mg/ | L or le | ess | | Biological treatment and adsorption not fruitful | | | |
| Toxin free water | | | | Biological treatment reduces 200-300 mg/L phenol to 0.5-1.0 | | | |
| | | | | mg/L | | | |
| | | | | | | | |

A. Batch Processes: The list of batch processes for their treatment is described as under.

1. <u>Separation by Steam Distillation</u>: The streams containing organics are generally treated for Phenol removal by steam distillation based on steam volatility of Phenol. In Phenol rich phenol-water mixture, drying of Phenol takes place in distillation process. This is applicable for dewatering columns in Phenol synthesis plants. Azeotropic distillation followed by steam stripping is a good process for purification of water from Phenol impurities. The azeotrope is split into Phenol rich phase which is recovered and water rich phase is refluxed into the system. The stripping/distillation column which works on this principle is shown in Figure 1. However, this process has huge energy requirement and high process cost.

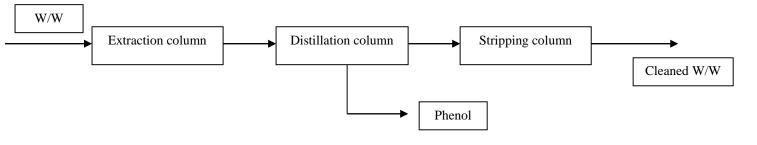


Figure 1 Schematic diagram of Phenol removal from wastewater using MIBK (Busca et al., 2008)

- 2. Separation by Extraction: Hydrocarbon and oxygenated organic solvents have the potential to extract Phenol from wastewater. Solvents used include benzene, toluene, n-hexane, acetate esters, diisopropyl ethers, methyl iso-butyl ketone etc (Pinto et al., 2005). Wastewater from distillation unit of Acetone crude in production of Phenol using cumene process containing Phenol in the range 1-3% are treated by extraction method. Cumene solvent is scrubbed of Phenol in a counter current caustic scrubber unit and the resulting sodium phenate solution is passed into a settling tank where cumene is recovered and recycled. The bottom of this tank is net result of all Phenol and its residual concentration goes up to 20-500 mg/L. The remaining Phenol is cleaned using biological processing. This process is combined with distillation for its efficient use. Phenol removal process was developed for coal gasification wastewater (Yang et al., 2005). For this extraction process, an appropriate solvent was prepared considering Phenol removal, solvent recovery and COD removal. It is one of the most important techniques when Phenol concentration in wastewater is high. Micro-organisms cannot survive when Phenol concentration is high hence biological treatment becomes difficult. Moreover, the presence of non-volatile dihydric and trihydric phenols is resistant to biological treatment. Therefore, a pre-treatment of coal gasification wastewater is particularly crucial. Extraction using four alternative solvents namely diisoprpyl ether (DIPE), butyl acetate, methyl isobutene ketone (MIBK), and 30% tributyl phosphate was investigated.
- 3. <u>Separation by adsorption:</u> Adsorption is a widely used technique for removal of Phenol from water. Various adsorbents used for adsorption are activated carbon, activated alumina, bentonite clays etc. Advantages of adsorption are simple column design and low installation which are cost effective. . In recent years, low cost adsorbents (locally available) having high binding towards the pollutant has been developed. Activated carbon is easily available and is commonly used as an adsorbent. Other conventional adsorbents used are bentonites (Banat et al., 2000), synthetic resins (Lin and Juang, 2011), polymer and polymeric based hybrid adsorbents (Pan et al., 2009) and alumina pillared clays (for removal of chlorinated phenols) etc. (Petrakis et al., 1998).

- a. Adsorption on activated carbon using agricultural waste: Activated carbon prepared from rubber seed coat (RSCC) which is an agricultural by product used as an adsorbent for Phenol removal from wastewater (Rengaraj et al., 2001). RSCC is used as a fuel and manure in Southern India. The studies show that it is a potential source for preparation of activated carbon since its Phenol removing capacity from aqueous solutions is 96% at prevailing conditions (Rengaraj et al., 2001). It can be used commercially for tertiary treatment of potable water and industrial effluents. Since commercial activated carbon is expensive, adsorbents are prepared from disposed wastes that are cheap and easily available. This serves two purposes; it is economical for the treatment plants to use recycled products and secondly it helps to dispose of the solid waste, which otherwise is a major cause of increased landfills. Substitute materials include straw, automobile tyres, fly ash, coal reject, sewage sludge, bagasse, fertilizer waste and saw dust. Due to high cost and variable performance of carbon regeneration, single use materials are desirable. Pine bark and apricot are used for making activated carbon and have also been used for Phenol removal from aqueous solutions.
- b. Adsorption using algae: Sargassum Muticum is commonly known as Japanese Wireweed. It is large brown seaweed of the genus called Sargassum (Rubín et al., 2006). Phenol, 2-chlorophenol and 4chlorophenol bio-sorption on Sargassum Muticum has been investigated.
- c. Pervaporation and Adsorption: Pervaporation, is a membrane process that separates a pure liquid or a liquid mixture when in contact with membrane on the feed or upstream side at atmospheric pressure and permeate is removed as vapour because of a low pressure existing on downstream side (Kujawski et al., 2004). This is an energy saving method in comparison to conventional methods. This enables to remove large quantity of Phenol from wastewater thereby purifying it to a greater extent. Using suitable organophilic membranes, pervaporation process can remove phenol effectively.
- d. Cross linked Cyclodextrin particles: Cyclodextrin particles are used as sorbents when wastewater contains 8.9% phenol, m- and p- cresols 0.33% and xylenes 0.44% (by weight). A series of sorbents are prepared by varying the composition of cyclodextrin, the cross-linker hexamethyl diisocyanate (HDI) or toluene 2, 6- diisocyanate and changing their molar ratio in the reaction batch. This process is instantaneous and is completed within 5 minutes. The best removal efficiency was obtained by the crosslinked -CyD with HDI in a 1:8 molar ratio or the crosslinked Mix-CyD with HDI in a 1:8 molar

ratio. The prepared sorbents were efficiently regenerated by elution of the adsorbed phenols from the crosslinked polymers with methanol (Yamasaki et al., 2006).

- 4. Electrochemical Treatment: Electrochemical method for water treatment is a versatile technique making purification of gases, liquids and solids possible and environmentally compatible. These are employed in removing naphthalene and anthraquinone sulphonic acids present in wastewater. However, use of suitable electrode is a matter of concern. The removal of these compounds has been done using Ti/Pt, Ti-Ru-Sn-SbO₂ and carbon felt (Panizza et al., 2000).
- *Electro-coagulation by iron electrodes*: It serves as an alternate technology for water treatment. The advantages are its in-situ delivery of reactive agents, secondary pollutants are not generated and compact equipment is used (Kobya et al., 2003).

B. Continuous process

1. Adsorptive Parameter pumping: A cyclic process based on the fact that adsorption equilibrium isotherms of solutes onto adsorbents are dependent on thermodynamic variables like temperature, pressure and pH etc. The two approaches for this process are: direct method, where in temperature change is imposed through the wall of the column and secondly when the temperature change is carried by the liquid stream. The advantage of this technique is its continuous mode of operation at low potential thermal energy as a regenerant thereby achieving a zero-pollutant plant (Ramalho et al, 1991).

3. Reactive Adsorption: Brief introduction

The coupling of a chemical reaction along with physical means of separation in a single unit operation is called Reactive Adsorption. Reactive adsorption can be carried out in two kinds of reactors namely: adsorptive reactors (AR) and chromatographic reactors (CR).

Realising the growing demand of energy and resource conservation, it is necessary to devise a treatment technology that is both economical and environment friendly. In the era of "more production with less energy" conventional unit operations have some disadvantages. Simple adsorption can be enhanced by coupling chemical reaction along with it and referred to as reactive adsorption. A reaction can be introduced into physical adsorption by two ways:

- 1. Crossing energy barrier of species to make them reactive by increasing either temperature or pressure.
- 2. Modifying adsorbent surface to provide a platform for reaction to occur.

Reactive adsorption (and its reverse, reactive desorption) resembles dissociative adsorption (and its reverse, associative desorption) but one fragment adds to an adsorbate rather than to a surface site (Compendium of Chemical Technology., 1997). Reactive adsorption is a process when adsorbate reacts with chemical specie (reactant) coated on the surface of an adsorbent and forms a product. Thus, in this case the product of adsorption interaction process is separated from the adsorbent. Reactive adsorption technique compared to simple physical adsorption has more potential to serve our purpose. The single unit of reactor-adsorber might reduce the design complexity and investment cost. It may also yield high purity products with reduced or eliminated downstream processing (Sharma et al., 2013). Although this technique is not new but a great deal of research has not been conducted till date.

4. Advanced Oxidation Processes (AOPs)

AOPs have become popular in recent years as an alternative for wastewater treatment. The basic principle of AOP's is degradation of pollutants by oxidation. These processes are defined broadly as aqueous phase oxidation processes based primarily on the formation of hydroxyl radical in the mechanism(s) which results in the destruction of the target pollutant or contaminant compound (Esplugas et al., 2002). The limitations associated include high cost of reagents such as ozone, hydrogen peroxide and source of light, ultraviolet radiation. However, costs can be reduced by using solar radiation as a source of energy. AOPs are best suited for pollutant degradation when biological treatments are not feasible (Esplugas et al., 2002).

4.1 **Chemistry of AOPs**

These processes have considerable similarities due to the presence of hydroxyl radicals participating in most mechanisms. The hydroxyl ions are extremely unstable and highly reactive. Therefore, kinetics seems to be first order with respect to OH ions and pollutant concentration. The reaction constant k value ranges from 10⁸ to 10¹⁰ M⁻¹s⁻¹. The concentration of radicals (at steady state) varies from 10⁻¹⁰ to 10⁻¹² M. Hence, the pseudo first order k is in the range of 1-10⁻⁴ s⁻¹ (Esplugas et al., 2002). These reactions are characterized by little selectivity of attack of the substrate and reaction conditions. AOPs offer different possible ways for production of hydroxyl ions thereby allowing a better compliance with the specific treatment requirements (Andreozzi et al., 1999).

AOP systems are classified as photochemical and non-photochemical depending upon the requirement of light for the reaction. In recent years, AOPs such as photo-catalyst, ozonation, photo-fenton, oxidation, ultrasound etc have been proposed for treating wastewater containing non-biodegradable or toxic substances in high concentration.

- 1. Fenton Oxidation: (Golbaz, 2013): Fenton agent used comprises of Fe²⁺ and H₂O₂ in acidic medium. Hydroxyl and ferrous ions both play an important role in enhancing the progress of the reaction according to the conditions like type of wastewater, ratio of Fe²⁺/H₂O₂ and presence of foreign substance.
- 2. Ozonation (Yang, 2012): The combined process of sonolysis and ozonation is one of the most effective methods in producing free radical ions. Since these processes are mass transfer limited in nature, this problem is overcome by the application of induced turbulence generated by ultrasound. In ozonation, various compounds can react with ozone via different ways. Firstly, they can react directly via molecular ozone and secondly indirectly via reactions with radical species (OH*, HO₂*), that are formed when ozone decomposes in water (Hoigné and Bader, 1975, 1976). On comparing it with reactive adsorption, ozonation is unselective and instant while the former is selective and may or may not be instantaneous. A transition state is achieved in RA where the product formed is detached from the surface of the adsorbent and no radical formation occurs. However, for molecular ozone reactions, selectivity and limitation towards degree of unsaturation, aromaticity, type of functional group, presence of double bonds etc are the factors affecting this process (Hoigné and

Bader, 1975, 1976).

- 3. <u>Electro-catalytic Degradation</u> (Zhou, 2002): These processes are used because of their amenability to automation, environmental compatibility and high efficiency. The degradation of phenol on various electrodes such as on PbO₂ and glassy carbon electrodes has been studied earlier.
- 4. <u>Catalytic wet oxidation processes</u> (Hussain, 2009): It is one of the most economically and technologically viable solution for treatment of wastewater when phenol concentration is increased to 20 mg/L. In this process, organic pollutants dissolved in water are partially degraded by means of oxidising agent into biodegradable intermediates or mineralised inorganic compounds such as CO₂, H₂O and inorganic salts. This process is carried out under high temperature and high pressure conditions. Metal oxides mixtures of Cu, Co. Mn, Zn, and Bi are used as catalysts in CWO. Both noble and metal oxides catalysts exhibit good properties in CWO.
- 5. <u>Electro coagulation process</u> (Abdelwahab, 2009): Electro-coagulation is a process of utilising sacrificed anodes forming active coagulants which removes pollutants using precipitation and floatation in situ. It can remove smallest colloidal particles.

This process occurs in a series of steps sequentially in the following order:

- Electrolytic reactions at electrode surface such as on Al surface, where Al ions are formed at anode and hydroxyl ions at cathode
- ii. In situ oxidation of Al ions and subsequent precipitation of aluminium hydroxide in aqueous phase
- iii. Adsorption of colloidal or soluble pollutants on coagulants that are removed by sedimentation and floatation

Table 2 Types of AOPs

| Name of AOP Process | Nature of Process | Remarks | Reference |
|---|---|--|--------------|
| 0 | Direct and redical math | Diverse magazina hatawa an | Early cos at |
| O_3 | Direct and radical path | Direct: reaction between | Esplugas et |
| | | ozone & dissolved | al., 2002 |
| | | compounds | |
| | | Radical path: reaction | |
| | | between radicals | |
| | | (produced due to ozone | |
| | | decomposition) & | |
| | | dissolved compounds | |
| O ₃ /H ₂ O ₂ | OH ⁻ generated by radical chain | Efficiency increases by | Esplugas et |
| | mechanism; interaction between O ₃ and | adding UV radiation | al., 2002 |
| | $\mathrm{H_2O_2}$ | | |
| | $H_2O_2 + 2O_3 \longrightarrow 2OH^* + 3O_2$ | | |
| UV radiation | Supplies radiation to chemical | Excited state, sufficient | Esplugas et |
| | compounds | time to promote reactions | al., 2002 |
| | | | |
| UV/O ₃ | Energy supplied by UV interacts with | High synergic effect | Esplugas et |
| | ozone | between ozone & UV | al., 2002 |
| | $H_2O + 2O_3 \xrightarrow{hv} 2OH^* + 3O_2$ | radiation separately | |
| UV/H ₂ O ₂ | Cleavage of molecule into two | Radiation with | Legrini et |
| | hydroxyl radicals formed per quantum | wavelength lower than | al., 1993 |
| | of radiation absorbed | 400 nm able to photolize | |
| | $H_2O_2 \xrightarrow{hv} 2OH^*$ | H ₂ O ₂ molecule | |

| $O_3/UV/H_2O_2$ | Increased fraction of ozone, enhanced | Fast and complete | Legrini et |
|-----------------|--|-----------------------------|-------------|
| | rate of ozone mass transfer in bulk | pollutant mineralisation, | al., 1993; |
| | liquid | most effective treatment | Esplagus et |
| | | for high polluted effluents | al., 2002 |
| | | | |
| | | | |
| Fenton reagent | Reaction between hydrogen peroxide | Incomplete mineralisation | Saritha et |
| | and iron (II) salts; iron considered a | of organic compounds | al., 2007; |
| | real catalyst | | Esplugas et |
| | $H_2O_2 + Fe^{2+} \longrightarrow Fe^{3+} + OH^* + OH^-$ | | al., 2002 |
| | (Acidic medium) | | |
| | | | |
| Photo-catalysis | In presence of artificial UV light and | Slow process, incomplete | Saritha et |
| | semi-conductor like TiO2 or ZnO | mineralisation of organic | al., 2007 |
| | | compounds | |

The combination of degradation and adsorption for phenols has been studied. Co/SBA-15 catalyst has been used for simultaneous adsorption and degradation of phenols (Sharma et al., 2013). Howsoever, technology feasibility and development of reactive adsorbents surfaces needs investigation for large scale industrial applications.

Table 3 gives a comparative study of the processes used for removal of phenol and its derivatives.

Table 3 Comparative studies on the techniques for phenol removal

| Treatment Technology | Principle/Reagent used | Advantages | Disadvantages | Reference |
|-------------------------|--|--------------------|------------------------|----------------|
| Distillation | Difference in steam | High process | High energy | Franck and |
| | volatility | efficiency | demands, expensive | Stadelhofer, |
| | | | technology | 1989 |
| | | | | Busca et al., |
| | | | | 2008 |
| Extraction | Difference in | Gives good results | Requires costly | Pinto et al., |
| | affinities of third | when practised | reagents as solvents | 2005; Busca et |
| | solvent with | with distillation | | al., 2008 |
| | solution to be | | | |
| | separated, C ₆ H ₆ , | | | |
| | Toluene, n-Hexane | | | |
| Activated | Physical adsorption, | Economic easy to | Expensive, pure | Busca et al., |
| Carbon | Activated carbon | install, easy | carbon incomplete | 2008, Freeman, |
| Adsorption | | regeneration | utilisation | 1995 |
| Adsorption | Physical Adsorption | Simple | Costly resin | Busca et al., |
| Resin | | installation, | production, | 2008 |
| | | operation | produces secondary | |
| | | | pollutants during | |
| | | | reactivation | |
| Oxidation with | O ₃ : Ozone | Effective phenol | TOC & COD not | Busca et al., |
| ozone | | removal | efficiently reduced as | 2008 |

| | | | intermediates are | Gimeno et al., |
|-----------------|--------------------------|---------------------|--------------------------|----------------|
| | | | formed | 2005 |
| | | | | |
| Oxidation with | TiO_2, H_2O_2, Fe^{2+} | Use of ferrate (VI) | Ferrate (VI) process is | Throop, 1975 |
| other Chemical | | dissociates phenol | slow, | & 1977, |
| Oxidants | | in environmentally | other oxidants not | Graham et al., |
| | | sound way | applicable as they | 2004 |
| | | | form toxic end | |
| | | | products | |
| | | | | |
| Photo Catalytic | - | Significant | High band width only | Gimeno et al., |
| Oxidation | | destruction of | part of the radiation is | 2005 |
| | | phenol | utilized | |
| | | | | |
| Bio Chemical | Sargassum | Inexpensive, | Requires more | Busca et al., |
| Abatement | Muticum: Japanese | environment | research, more | 2008 |
| | wireweed, brown | friendly | dilution is needed | Lond Jang et |
| | algae | | since phenol is toxic | al., 2006 |
| | | | to microbes | Shetty et al., |
| | | | | 2007 |
| | Al or Fe electrodes | | | |
| Electro- | | In-situ delivery of | Sludge formation | Kobya et al., |
| chemical | | reactive agents, no | | 2003 |
| Process | | generation of | | |
| | | secondary | | |
| | | pollutant and | | |
| | | compact | | |
| | | equipment | | |
| | | | | |

| | Membrane | | | |
|----------------|---------------------|-------------------|----------------------|------------------|
| | separation | Greater extent of | | |
| Pervaporation | | purification | Membrane fouling | Kujawski et al., |
| and adsorption | | obtained, energy | | 2004 |
| | | saving method | | |
| | | | | |
| | | | | |
| | Continuous process, | | | |
| Parameter | change brought | - | | |
| Pumping | about by changing | | Parameter | Mishra et al., |
| | temperature, | | optimisation is a | 2007 |
| | pressure, pH | | problem | |
| | | | | |
| | | | | |
| | Reactive surface of | | | |
| | adsorbent | | | |
| Reactive | | No separate step | | |
| Adsorption | | for regeneration | Selective in nature, | Sharma et al., |
| | | | not instantaneous | 2013 |
| | | | | |

For effective adsorption process, adsorbent must be regenerated without losing its adsorption capacity. Desorption is achieved either by causing variation in temperature or pressure or through displacement with another compound with higher affinity. Among different available regeneration techniques, the selection depends on economics and technical considerations of the reaction systems (Sharma et al., 2013).

5. Regeneration of spent adsorbent

Adsorbents that are widely used for adsorption of Phenol from wastewater become saturated after prolonged usage. Hence, these must be regenerated after fixed or non-fixed duration of time since it is the only solution which is economical and feasible (Castilla et al., 1995).

The most commercially used adsorbent worldwide is activated carbon. A typical diagrammatic flowchart below represents the techniques used to regenerate a spent adsorbent.

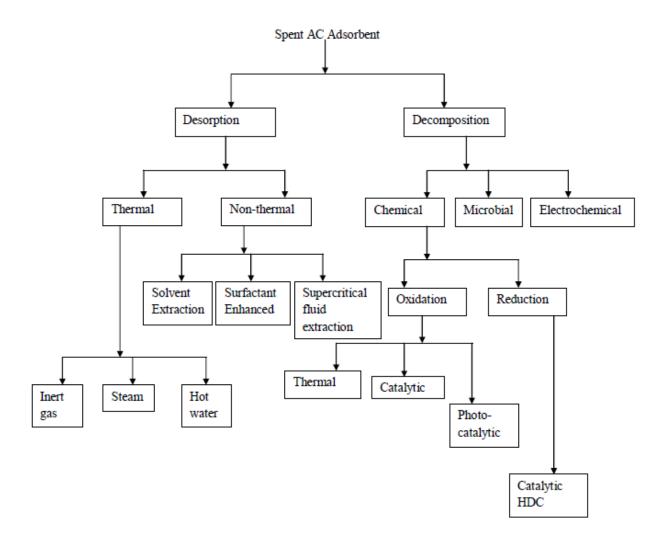


Figure 2 Overview of techniques for regeneration of Activated Carbon (Meytal and Shientuch., 1999)

There are several methods of regenerating a spent adsorbent. Some of them are discussed below"

1. <u>Electrochemical Regeneration</u>: This process is used for regeneration of activated carbon saturated with p-nitrophenol (PNP) (Zhou and Lei, 2006). A non-active electrode modified PbO₂ electrode was used which generated hydroxyl radical ion effectively and was able to maintain stable performance for organic wastewater treatment. Its service life is expected to be 10.4 years under the application of current density of magnitude 0.1 A/cm² and strong acidic solutions (9 M H₂SO₄) (Zhou and Lei., 2006).

This method has also been used for regenerating activated carbon made of coconut shell exhausted with phenol (Zhang, 2000).

- 2. <u>Thermal Regeneration</u>: This involves following procedure: (1) drying at 150°C, (2) pyrolysis under inert atmosphere and (3) gasification of residual organics, by oxidising gas, like steam or CO₂. In the recovery of activated carbon exhausted with p-nitrophenol, thermal regeneration is done through three methods: (1) Pyrolysis (2) Pyrolysis-Gasification and (3) Direct gasification. The gasifying agents are water and CO₂ (Sabio et al., 2004).
 - a. *Thermal regeneration at high pressure*: A new procedure to recover activated carbon is a combination of thermal desorption with water at high temperature and pressure (150 atm and 623K) in complete absence of oxygen (Utrilla et al., 2002).
- 3. <u>Electrochemical Regeneration</u>: This technique has been used to recover spent granular activated carbon because of its certain unique features such as: low temperature operation, no chemical added and in-situ cracking of organics deposited on carbon surface without damaging the structural properties and characteristics of carbon (Wang and Balasubramanian, 2009).

Table 4 A comparative study of various regeneration processes of spent activated carbon are described below

| Treatment Technology | Principle / Reagent used | Operating Conditions | Advantages | Disadvantages | Reference |
|-------------------------|-----------------------------|-------------------------|-------------------|------------------|------------------|
| Thermal | Drying, thermal | 700-1000°C | Simple process | Continuous loss | Meytal and |
| Regeneration | desorption and | | applicable to all | of 5-15% per | Shientuch., |
| | high temperature | | regeneration | cycle in | 1999 |
| | reactive treatment | | processes | adsorption | |
| | in inert gas | | | capacity carbon | |
| | | | | surface area | |
| Extractive | Use volatile | - | - | - | Meytal and |
| Regeneration | solvents | | | | Shientuch., |
| | | | | | 1999 |
| Surfactant enhanced | Flushing | Miscelles formed | Adsorption | Expensive, | Meytal and |
| regeneration | concentrated | consisting 50-100 | capacity over | environmentally | Shientuch, 1999 |
| | surfactant solution | molecules | 50% observed on | unacceptable | |
| | through spent AC | | virgin AC | | |
| Chemical | Complete | - | - | Not feasible for | Meytal and |
| regeneration | conversion of | | | continuous | Shientuch, |
| | adsorbed species | | | processes, not | 1999; Utrilla et |
| | to harmless | | | economically | al., 2002 |
| | products/ Oxidants | | | viable | |
| | used Chlorine, | | | | |
| | | | | | |
| | peroxide, chlorine | | | | |

| © 2016 IJRAR | March 2016, Volume 3 | s, issue 1 w | ww.ijrar.org (E-155) | N 2348-1269, P- ISSN | 2349-5138) |
|--------------------|--|-------------------|----------------------|----------------------|------------------|
| Photo-Catalytic | TiO ₂ , SnO ₂ , ZrO ₂ | - | - | Long process | Meytal and |
| Regeneration | used in presence of | | | hence not | Shientuch, 1999 |
| | UV light | | | practically | |
| | | | | possible | |
| Reductive | Catalytic HDC | - | Still under | - | Meytal and |
| Treatment | using reductants | | development | | Shientuch, 1999 |
| | like H ₂ and NaBH ₄ | | stage | | |
| | or H_2 and N_2H_4 | | | | |
| Microscope induced | Microwave | Microwave output | Requires short | Input power of | Ania et al., 200 |
| regeneration | regeneration | power is 2000 W | period of time, | microwaves need | |
| | | at 2450 MHz, | lower | to be increased | |
| | | single mode | consumption of | when samples are | |
| | | cavity where | gas energy, | saturated | |
| | | sample is exposed | preserves the | | |
| | | to microwave | porous structure, | | |
| | | heating | increased | | |
| | | | adsorption | | |
| | | | capacities, | | |
| | | | carbon can be | | |
| | | | recycled and | | |
| | | | reused a large | | |
| | | | number of times | | |
| Ozone regeneration | Ozone as oxidizing | Room temperature | Removes both | Restoration of | Álvarez et al., |
| | gas | | physically and | surface area | 2004 |
| | | | chemically | depends on | |
| | | | adsorbed phenol | ozonation time | |
| | | | | | |

| | | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | | | |
|-------------------|---|--|-------------------|--------------------|-----------------|
| | | | from carbon | GAC itself, | |
| | | | surface, restores | ozonation beyond | |
| | | | most of its | optimum time | |
| | | | surface area | gives rise to a | |
| | | | | slightly decreased | |
| | | | | surface area | |
| | | | | | |
| High pressure and | Liquid water at | 623 K and 150 | No oxidation of | Slight destruction | Utrilla et al., |
| temperature | high pressure and | atm in absence of | Carbon; no | of mesopores and | 2002 |
| | temperature | oxygen | losses of carbon | opening of | |
| | | | during treatment, | micropores and | |
| | | | consumes less | macropores, | |
| | | | energy than | Regenerated | |
| | | | thermal | sample has | |
| | | | regeneration | decreased surface | |
| | | | | area and pore | |
| | | | | volume | |
| | | | | | |
| Electrochemical | Uses SnO ₂ /Ti | Semi batch | Environmental | - | Wang and |
| Regeneration | anodes and 5 % | electrochemical | compatibility, | | Balasubramania |
| | Na ₂ SO ₄ solution as | reactor operating | versatility, | | n, 2009 |
| | electrolyte | under wide | energy and cost | | |
| | | conditions | efficient, | | |
| | | | amenability to | | |
| | | | automation | | |
| | | | | | |
| | Uses two Platinum | NaCl, Na ₂ CO ₃ , | | - | Zhang, 2002 |
| | electrodes | NaHCO ₃ , Na ₂ SO ₄ | | | |
| | | | | | |

| | as electrolytes | NaCl has high | | |
|---------------------------|--------------------|-----------------|--------------------|---------------|
| | (1%), 50 mA | regeneration | | |
| | current | efficiency | | |
| | density,25°C for 5 | | | |
| | h | | | |
| | | | | |
| Anode: β-PbO ₂ | NaCl as | | | |
| modified with | electrolyte, | | Slight decrease in | Zhou and Lei, |
| fluorine resins | 25±0.5°C for 30- | | micropore volume | 2006 |
| | 120 min, fluidised | AC effectively | | |
| | electrochemical | regenerated | | |
| | reactor | within 1.5 h | | |
| | | without much | | |
| | | change in pore | | |
| | | structure, cost | | |
| | | effective | | |
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The present review covers description of removal techniques of phenols from wastewater. There has been a growing demand to devise an eco-friendly and economically feasible method for wastewater treatment owing to the hazardous and toxic nature of the phenolic compounds and their derivatives. The study compares various conventional and latest methodologies for the same.

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